A Geometric Approach
to Group Delay Network Synthesis

Piotr Jan OSUCH, Tinus STANDER

Dept. of Electrical, Electronic and Computer Engineering, University of Pretoria, Lynnwood Road, Pretoria, South Africa

{piotr.osuch, tinus.stander}@up.ac.za

Abstract. *All-pass networks with prescribed group delay are used for analog signal processing and equalization of transmission channels. The state-of-the-art methods for synthesizing quasi-arbitrary group delay functions using all-pass elements lack a theoretical synthesis procedure that guarantees minimum-order networks. We present an analytically-based solution to this problem that produces an all-pass network with a response approximating the required group delay to within an arbitrary minimax error. For the first time, this method is shown to work for any physical realization of second-order all-pass elements, is guaranteed to converge to a global optimum solution without any choice of seed values as an input, and allows synthesis of pre-defined networks described both analytically and numerically. The proposed method is also demonstrated by reducing the delay variation of a practical system by any desired amount, and compared to state-of-the-art methods in comparison examples.*

Keywords

All-pass circuits, approximation problem, analog signal processing, delay ripple equalization, group delay engineering, linear phase filters

1. Introduction

The ever-increasing performance requirements of modern high-speed communication systems favor analog solutions for real-time signal processing applications. At high frequencies (such as millimeter-wave frequencies) analog devices outperform their digital counterparts in terms of cost, power consumption and the maximum attainable bandwidth [1]. Furthermore, the digitization process of future wideband channels (such as the International Telecommunication Union 71–76 and 81–86 GHz bands) requires sampling speeds of at least 10 GSPS, currently achievable at the cost of sacrificing resolution and dynamic range [2]. The fundamental building block of any analog signal processor is a delay structure [3–5] of prescribed response. This quasi-arbitrary group delay function can be synthesized by cascading all-pass sections to obtain a delay function approximating the required response to within a constant. This synthesized network may then either be inserted in a system stand-alone to perform an analog signal processing function, or cascaded with an existing network to reduce the group delay variation of the resulting combined system. This approach is compatible with several existing techniques [1], [6–12] for the synthesis of group delay networks.

Initial methods for synthesizing continuous group delay functions (using analog all-pass networks) were aimed at reducing the group delay variation of color television receivers [11]. These methods typically assume the form of design tables and graphs, as well as trial and error design approaches and are therefore limited to particular applications.

In an effort to address these limitations, analytical techniques for synthesizing the group delay of an electrical network have been developed [3], [4], [10], [13–15]. Of these, only one presents a rigorous theoretical treatment to finding minimal-order solutions to the synthesis problem [13]. This is done by approximating the original system's group delay characteristic, to within a specified error, using the real Fourier series with an optimal number of all-pass sections. In this method, convergence of the system of analytical equations is, however, sensitive to both the original group delay function and the choice of initial solutions, often failing to converge for practical cases [13]. This method is also limited to the low-pass case and provides poor convergence if the bandpass signal is treated as an extended low-pass spectrum [7], [8]. The approach presented in [3], [4] solves the approximation problem by generating a Hurwitz polynomial, with the desired phase response, at specified frequencies, which are chosen a priori. No rigorous method of choosing these frequency points, such that the resulting solution is minimal-order, is presented.

Due to these problems with state-of-the-art analytical synthesis methods, numerical approaches relying on optimization algorithms have been widely sought in the modern group-delay synthesis literature [1], [5], [6], [14–17]. The most popular approach [14] is based on approximating a desired group delay curve with a summation of second-order all-pass networks to within an arbitrary additive

constant. The theoretical approximation is expressed in terms of nonlinear constraints at specific points that are then perturbed to achieve quasi-equi-ripple convergence. Convergence of this method is sensitive to the chosen initial value set, though this shortcoming is partially alleviated by a trial-and-error approach. This method also fails to account for deviations of practical realizations from theoretical models, which are of particular importance in the design of high-frequency systems [18]. A similar approach is presented in [15], with the exception that the imaginary components of the all-pass poles and zeros are assumed to be the frequency locations of the local maxima of the resulting delay curve. As with the method in [14], it is impossible to analytically determine the initial solution set which guarantees convergence. Other approaches using the differential evolution and genetic algorithms [1], [6], [16] have also been proposed. Such approaches tend to be computationally intensive and are prone to converge to local minima, as opposed to a global optimum.

In this work, we present a new numerical synthesis procedure of minimum-order series-cascaded all-pass networks having a quasi-arbitrary group delay response, making the following contributions to the state-of-the-art:

1) Our method does not require an initial value set. Convergence is therefore not dependent on an appropriate selection.

2) The resulting group delay function is an approximation of the required response to within any arbitrarily specified maximum delay variation across the passband, extending on methods in literature [3–6], [10], [13], [14] where the network's order is chosen and not, explicitly, the resulting maximum delay variation.

3) The method is implementation abstracted, in that any theoretical, circuit, or parametrized numerical model description of a second-order all-pass section can be applied in the algorithm.

4) Due to the underlying analytical nature of the approach, rapid convergence is achieved; typically within 20 iterations for practical cases (as will be shown in the examples). This is an order of magnitude fewer iterations required by more general state-of-the-art optimization methods (genetic algorithm and simulated annealing), as is shown in comparative examples.

To maintain generality, this paper only considers second-order all-pass sections with complex poles and zeros, of which a special case is the first-order network centered around zero frequency.

This paper is organized as follows. First, the problem of synthesizing a quasi-arbitrary group delay function is formulated geometrically on the complex s-plane and a derivation of the algorithm is presented. The proposed method is then demonstrated by synthesizing a linear group delay function with a sixth-order theoretical all-pass network. Next, in order to demonstrate the flexibility of the

algorithm, Gaussian and higher-order delay functions are synthesized, followed by an example synthesis of a network to reduce the variation in group delay response of a physically measured system (in this case, a fifth-order hairpin resonator BPF). Lastly, the proposed method is compared to existing techniques in the literature and the improvements are demonstrated. The synthesized all-pass networks are implemented in lumped-element [9] form. In all cases, National Instruments AWR Microwave Office 10 is used as the circuit simulator.

2. Theory of Group Delay Synthesis

2.1 Approach

The group delay, as a function of frequency, of an ideal second-order all-pass network, may be expressed in terms of the quadrature all-pass pole/zero pair locations, by the relationship [13]:

$$\tau_{\text{quad},x}(\omega) = 2\sigma_x \cdot \left[\frac{1}{(\omega + \omega_x)^2 + \sigma_x^2} + \frac{1}{(\omega - \omega_x)^2 + \sigma_x^2} \right] \quad (1)$$

where σ_x and ω_x represent the values of the Re and Im components of the poles and zeros respectively, on the $\mathbb{C}$ s-plane. A quasi-arbitrary group delay function can be synthesized indirectly by cascading all-pass sections as described by (1) with a cost function τ_c (chosen to have the negative of the required delay curve) to obtain a cascaded response referred to as an error function τ_e. Then, by minimizing the variation of τ_e, the resulting all-pass network's delay τ_s approximates the required response to within a constant. Reducing the variation of an arbitrary continuous group delay function τ_e by means of cascaded all-pass sections can be expressed mathematically as:

$$\tau_e = \min \left\{ \Delta_{\max} \left\{ \tau_c + \underbrace{\sum_{x=1}^{N} \tau_{\text{quad},x}(\omega)}_{\tau_s} \right\} \right\} \quad (2)$$

where the order of the all-pass network is 2N, $\Delta_{\max}$ represents the maximum variation in the passband of interest and min is a numerical minimization algorithm. This is further illustrated in Fig. 1. The delay cost function τ_c can either represent the negative of the desired function (by reducing the variation $\Delta_{\max}$, an approximation to the desired function is then synthesized) or a practical system that is to be equalized.

As per the introductory discussion, a theoretical basis is desired for finding the N initial solution sets (σ_x, ω_x), which ensure that (2) converges to a global optimum.

Our approach in this paper simplifies the complexity of the minimization problem described in (2) by using a novel geometrical approximation to the ideal all-pass network of (1), subsequently leading to an approximate analy-
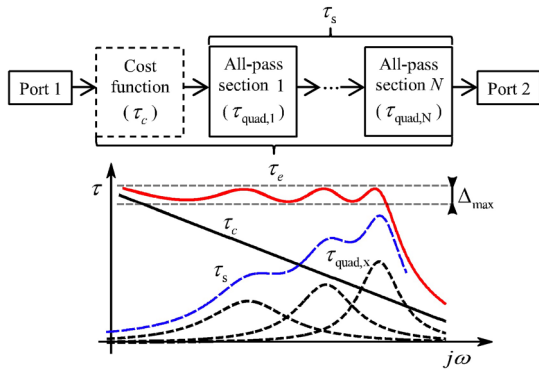
Fig. 1. All-pass network cascaded with the cost function.

Fig. 2. Graphical illustration of theorem 1.

tical solution to (2) in the form of initial all-pass pole/zero solution intervals. These intervals are found in such a way that (2) is necessarily monotonic over each interval and, as a result, any gradient-based optimization will always converge to a solution. The end result is either an equi-ripple solution (if at all possible for the given delay function and desired maximum variation) or a solution with the fewest local minima and maxima, both of which are optimal results [14].

After an initial solution is found using the approximation to (1), it is replaced with the more accurate all-pass network descriptions of (1) and subsequently numerically optimized in the knowledge that, by the preceding step, a global optimum solution will be found. This results in an all-pass network composed of ideal all-pass quadrature pairs. The ideal all-pass quadrature pairs are then individually implemented in the passband of interest by using theoretical, circuit-simulated or otherwise parameterized numerical descriptions of practical all-pass networks [9]. The individual second-order circuit blocks are then optimized to achieve 1:1 equivalence with the theoretical all-pass section, they are to represent in the circuit, and then cascaded with the original network without further optimization.

2.2 Theoretical Derivation

We will first find a simplification to (1) as mentioned above. Equation (1) may be simplified by assuming that $\omega_x \gg BW/2$ and by removing the negative frequency pole/zero pair, without appreciably affecting the group delay curve at positive frequencies, where BW is the bandwidth of interest. Next, using the additive property of differentiation and the symmetry of the pole/zero pair about the Im jω-axis, it can be shown that the group delay of a single pole and a pole/zero pair is equivalent, provided that:

$$p_x = \left\langle -\sigma_{px}, \omega_{px} \right\rangle \rightarrow \begin{cases} p_x = \left\langle -2\sigma_{px}, \omega_{px} \right\rangle \\ z_x = \left\langle +2\sigma_{px}, \omega_{px} \right\rangle \end{cases} \quad (3)$$

where p_x and z_x are the locations of the xth pole and zero pair, respectively. An approximation to (1) can therefore be found by approximating the group delay of a single pole in
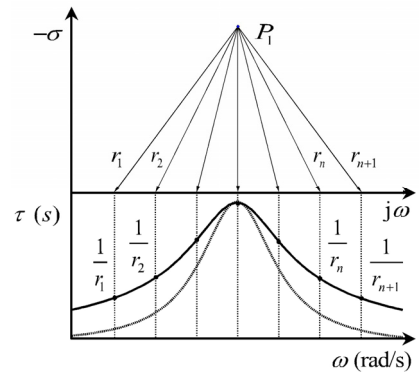
the II quadrant of the s-plane, as described by theorem 1 below. The derivation is presented in Appendix 1.

Theorem 1. *Assume that a single pole exists in the II quadrant of the complex s-plane at point P_1. Further assume that τ is the group delay caused by the pole at P_1 at a frequency $\omega = P_2$ where P_2 is any point on the positive Im jω-axis of the s-plane. Then:*

$$\tau \approx \frac{1}{\overline{P_1 P_2}} \quad (4)$$

where the error of the approximation is:

$$\lim_{P_2 \to \text{Im}\{P_1\}} \left[\tau - \frac{1}{\overline{P_1 P_2}} \right] = 0 . \quad (5)$$

Theorem 1 is demonstrated graphically in Fig. 2 where the error of approximation approaches zero as τ approaches its maximum. This relationship forms the basis of the synthesis algorithm presented in this paper.

Having derived an approximation to (1) the problem of (2) can be solved. To realize a final cascaded system τ_e (Fig. 1) with equi-ripple variation in group delay, appropriate selections for $\tau_{quad, x}$ must be made. Since τ_c is assumed to be a piecewise smooth function, the introduction of $\tau_{quad, x}$ to satisfy (2) necessarily implies the introduction of new local minima and maxima to τ_e. Furthermore, by the equi-ripple requirement, a local minimum must be followed by a local maximum. The minimization problem can therefore be restated as: finding optimal locations for new local minima in τ_e, while simultaneously controlling the peaks of resulting subsequent local maxima, such that the desired maximum p-p delay variation of τ_e is obtained.

An algorithm is developed for introducing such local minima and maxima with second-order all-pass networks, whereby a sequence of iterations successively introduces new poles p_x in the II quadrant of the s-plane, until the desired peak group delay variation in (2) is obtained. These poles are then later replaced by quadrature all-pass pairs as per the transformation of (3), to preserve the initial system's magnitude response.

To introduce a new local maximum or minimum at a specific frequency of the group delay function τ_e, a pole

must be placed on a semi-circular curve on the s-plane, as described by the following theorem which is derived in Appendix 1.

Theorem 2. *Assume that $\tau_e(\omega)$ represents the group delay of some system of interest. Suppose that a local maximum or minimum is required at $\omega = \omega_{mx}$. Then a new pole p_x must be placed in the s-plane anywhere on the curve $\overrightarrow{r_{px}(\beta_x)}$ where β_x is the angle with the $+j\omega$-axis and*

$$r_{px} = \sqrt{\frac{\cos(\beta_x)}{c_1}} \qquad (6)$$

where:

$$c_1 = -\frac{\partial}{\partial \omega}\left[\tau_e(\omega)\right]\Big|_{\omega=\omega_{mx}} . \qquad (7)$$

The location of p_x, as expressed in terms of rectangular coordinates, in a right hand coordinate system is equivalently:

$$\overrightarrow{r_{px}(\beta_x)} = \left\langle \omega_{px}, -\sigma_{px} \right\rangle = \left\langle \cos(\beta_x)r_{px} + \omega_{mx}, -\sin(\beta_x)r_{px} \right\rangle.$$

Theorem 2 is illustrated in Fig. 3.

As β_x is traversed from $\pi/2$ to 0, the maximum peak delay value introduced by p_x first decreases (since the perpendicular distance from p_x to the Im $j\omega$-axis increases) and then increases again (after the apex of the semi-circle is traversed), as per theorem 1. The introduced delay value therefore begins and ends at ∞. When $\beta_x > \beta_{cx}$, ω_{mx} is a local maximum and as β_x decreases ω_{mx} transforms to a local minimum exactly once (see Appendix I for derivation), where β_{cx} can be found by:

$$c_2 = \frac{\left[3\cos^2(\beta_{cx})-1\right]\left[c_1\right]^{3/2}}{\left[\cos(\beta_{cx})\right]^{3/2}}. \qquad (8)$$

The foregoing discussion is further illustrated with Fig. 4.

The next step involves selecting one pole from the infinite set of allowed values for p_x, with $\beta_x < \beta_{cx}$, such that the local maxima preceding (at $\omega = \omega_{lx}$) and succeeding (at $\omega = \omega_{rx}$) the newly introduced local minimum are both equal in magnitude and not greater from the local minimum than by the maximum allowed variation value, Δ_{max}, as further illustrated in Fig. 5:
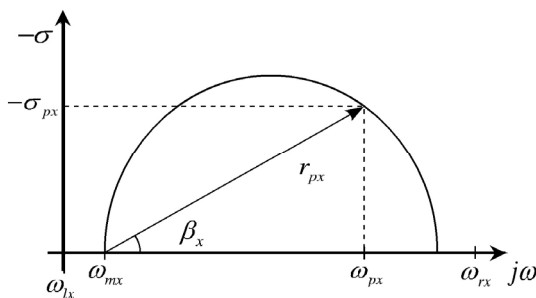

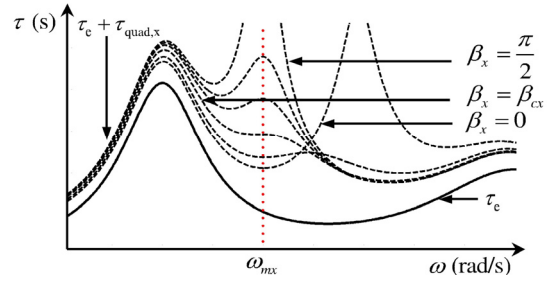**Fig. 3.**   Graphical illustration of theorem 2 on the s-plane.

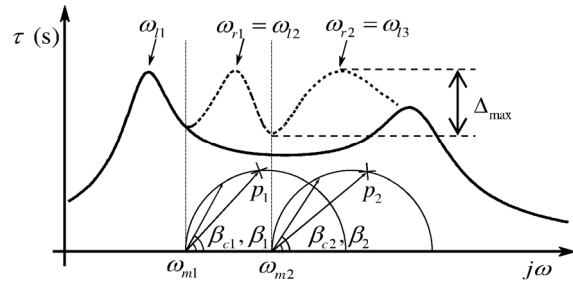**Fig. 4.**   Graphical illustration of theorem 2 in the frequency-time domain.

Fig. 5.   Graphical illustration of the group delay synthesis algorithm.

$$\tau_e(\omega_{lx}) - \tau_e(\omega_{mx}) = \Delta_{max} , \qquad (9)$$

$$\tau_e(\omega_{rx}) - \tau_e(\omega_{mx}) = \Delta_{max} . \qquad (10)$$

Before solving for ω_{mx} and β_x the behavior of the group delay at any point other than at ω_{mx}, as β_x changes in Fig. 3, is found to be:

$$\tau(\omega) = \tau_e(\omega) + \left\{\left(\omega - \omega_{mx} - \cos(\beta_x)r_{px}\right)^2 + \left(\sin(\beta_x)r_{px}\right)^2\right\}^{-\frac{1}{2}}. \qquad (11)$$

The solution to (9) and (10) is split into two parts; first ω_{mx} is found by assuming $\beta = \beta_{cx}$ and solving (9); then β_x is found by solving (10). Substituting (11) into (9) it can be shown that:

$$\Delta_{max} = \tau_e(\omega_{lx}) - \tau_e(\omega_{mx}) +$$
$$\left\{\left(\omega_{lx} - \omega_{mx} - \cos(\beta_x)r_{px}\right)^2 + \left(\sin(\beta_x)r_{px}\right)^2\right\}^{-\frac{1}{2}} - \frac{1}{r_{px}}. \qquad (12)$$

Since (12) has an impractically lengthy analytical solution and since τ_e may be numerical in nature, a numerical solution is justified. An interval for ω_{mx} where a *unique* solution can exist is found thereby systematizing the numerical approach:

$$\omega_{mx} \in \left(\omega_{lx} : \omega_{mx(max)}\right) \qquad (13)$$

where $\omega_{mx(max)}$ is the first zero crossing of c_1 (itself a function of ω_{mx}) greater than ω_{lx}. A simple numerical root-finding algorithm is used to solve for ω_{mx} in the interval of (13). The next step is that of finding β_x such that (10) is satisfied. Similarly to the previous discussion, (11) is substituted into (10) and β_x is found using numerical root-finding methods in the interval:

$$\beta_x \in \left(\beta_{cx} : 0 \right). \tag{14}$$

This step concludes solving (9) and (10) for the xth pole, p_x. Through a sequence of iterations, τ_c is traversed over the entire bandwidth starting from the band edge with the larger group delay, resulting in the desired variation over the entire band of interest. Each new p_x reduces the delay variation to the specified maximum value, over a portion of the bandwidth, $\omega \in [\omega_{lx} : \omega_{rx}]$. This procedure is illustrated in Fig. 5, where two poles are introduced, starting at the lower frequency band edge.

We summarize the synthesis unit step as shown in the flow diagram of Fig. 6.
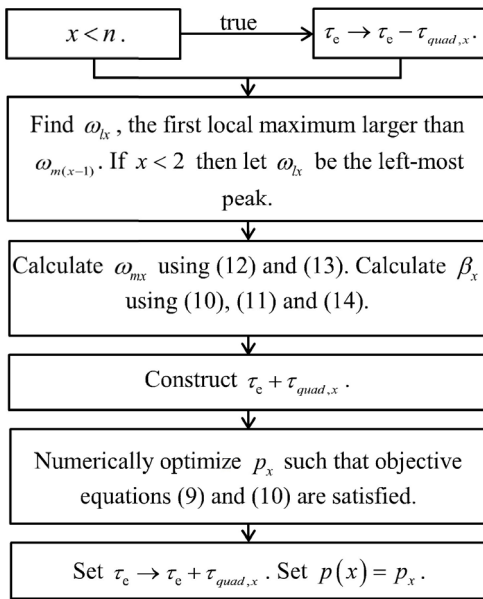
Fig. 6. The synthesis unit step (S(x)).

Vector $\vec{p}$ is the collection of all n poles p_x calculated thus far in the progression of the algorithm. For brevity, only traversal starting at the lower frequency band edge is described. The unit step is used *iteratively* by the main algorithm of Fig. 8, both to introduce new poles and also to re-synthesize previously calculated poles. To simplify notation, the unit step is represented by the functional block of Fig. 7. In Fig. 8, q is set as the maximum allowed fractional variation between iterations of p_x, allowing for a successful termination of the algorithm.

If the left- and right-most peaks of the group delay are approximately equal, equations for finding ω_{mx} and β_x, in certain cases, have no solution (for the desired maximum variation). This problem can be averted by simply raising/pre-distorting one band edge with an additional pole before proceeding with the algorithm of Fig. 8.

Finally, each individual $\tau_{\text{quad},x}$ may be replaced by a more accurate parametric or numerical description of the delay element, provided that the delay function can be approximated by (1).
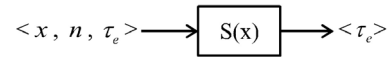

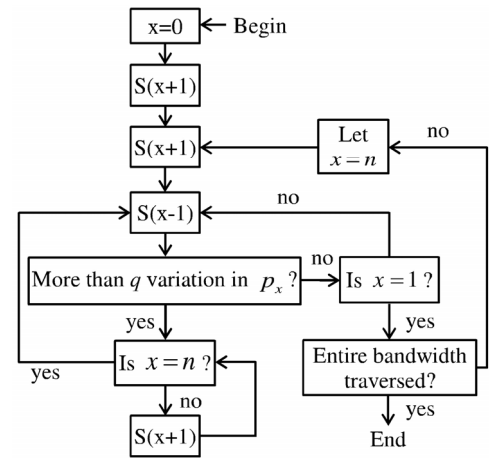**Fig. 7.** Synthesis unit step function block diagram.

Fig. 8. Proposed numerical group delay synthesis algorithm.

3. Application Examples

3.1 Example 1: Synthesis of a Linear Group Delay Function

We now demonstrate the proposed algorithm of Fig. 8 by synthesizing a network with a linear increase in group delay from 2 ns to 4 ns, as may be required when implementing a Fourier transform [1]. This can be done by reducing the variation of the negative of the desired response (cost function) over the desired passband, as illustrated in Fig. 9.

The initial peak group delay variation of τ_e is 2000 ps and the desired final variation is set to 300 ps. From Fig. 9, $\omega_{l1} = 1.256 \times 10^{10}$ rad/s and by using (12) and (13) it is found that $\omega_{m1} = 1.618 \times 10^{10}$ rad/s with $\beta_{c1} = 0.9553$ rad. Then (10), (11) and (14) are used to calculate $\beta_1 = 0.4286$ rad. The initial starting location for p_1 is therefore $(-\sigma_1, \omega_1) = (0.994, 17.790) \times 10^9$. This value is then optimized numerically using a simple monotonic gradient-based optimizer (no longer using the approximation of
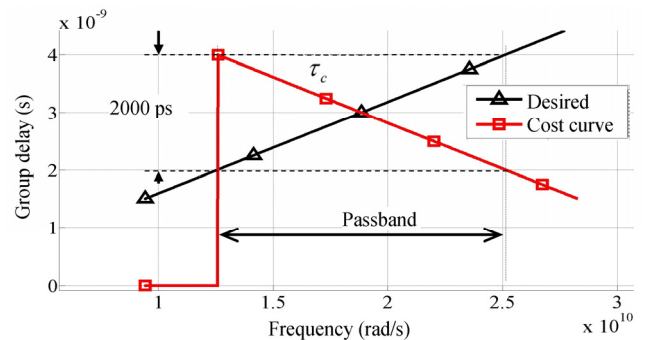

Fig. 9. Desired linear group delay and cost function.

Variable of interest	Iteration				
	1 (p_1)	2 (p_2)	3 (p_1)	4 (p_2)	5 (p_3)
ω_{lx} / 10^{10} rad/s	1.2557	1.8067	1.2576	1.8085	2.1878
ω_{mx} / 10^{10} rad/s	1.6180	2.0293	1.6387	2.0878	2.3519
β_{cx} / rad	0.9553	1.0035	0.9860	0.9892	1.0051
β_x / rad	0.4286	0.5410	0.4636	0.5310	0.5830
$p_{,initial}$/ 10^9	(0.994,17.790)	(0.703, 21.132)	(1.145, 17.782)	(0.766, 21.765)	(0.581, 24.155)
$p_{,optimized}$/ 10^9	(0.995,18.397)	(0.697, 21.561)	(1.188, 18.698)	(0.764, 22.151)	(0.581, 24.482)

Tab. 1. First five iterations of the group delay synthesis algorithm.

Theorem 1 in (2)) and found to be $(-\sigma_1, \omega_1) = (0.995, 18.397) \times 10^9$.

The aforementioned results are summarized in Tab. 1. The first unit step is concluded with the desired variation satisfied over the interval $\omega \in [\omega_{l1} : \omega_{r1}] = [1.26:1.82] \times 10^{10}$ rad/s, as shown in Fig. 10. We repeat the unit step procedure as per the algorithm of Fig. 8. The second unit step is concluded with the desired delay variation satisfied over the interval $\omega \in [1.83 : 2.14] \times 10^{10}$ rad/s, as shown in Fig. 11. The next step involves removing a previously synthesized pole and recalculating its position as per the modification $\tau_e \rightarrow \tau_e - \tau_{quad,x}$ shown in Fig. 6. Figure 12 shows the group delay profile after this subtraction is performed.

We now repeat the unit step procedure and re-compute the erased pole as shown in Tab. 1 under iteration three. A comparison of iterations one and three reveals the improvement in the approximation of the location of pole p_1. The group delay synthesis algorithm repeats in this manner until the values of p_1, p_2 and p_3 converge (the threshold is set at $q = 3\%$, which is arbitrarily chosen).
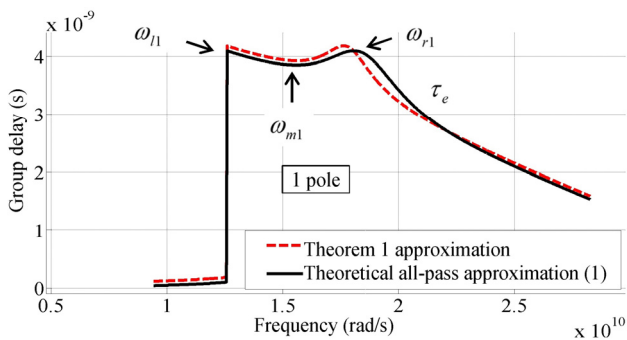
For brevity, all iterations are not shown in detail. The algorithm ends after 9 iterations with the final cascaded error group delay shown in Fig. 13. By removing the cost function response τ_c, the resulting synthesized linear group delay function τ_s is shown in Fig. 14. Convergence of the three poles is shown in Fig. 15.
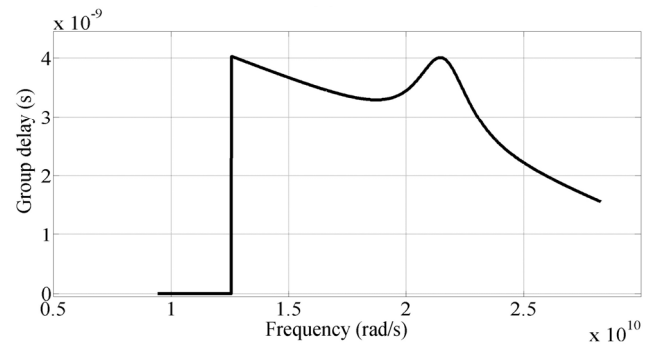

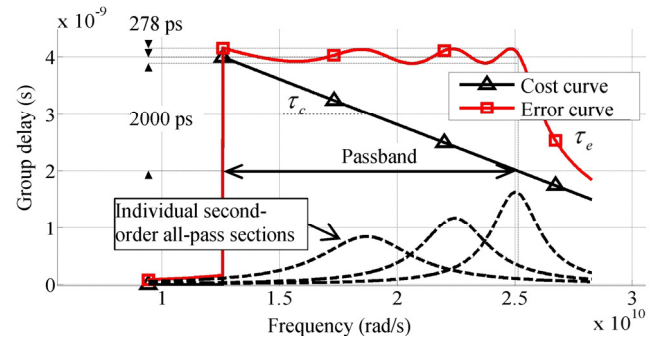**Fig. 12.** Iteration 3 of the delay synthesis algorithm – removal of pole p_1.

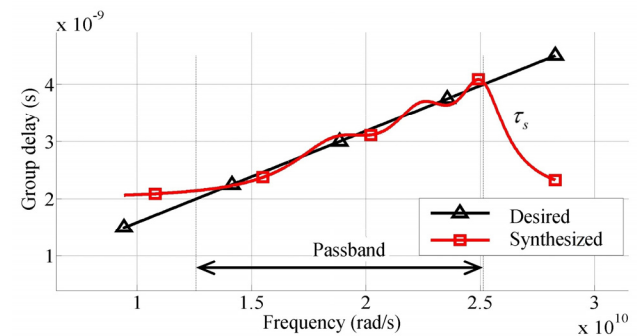**Fig. 13.** Cost and error delay functions.

Fig. 10. Iteration 1 of the delay synthesis algorithm.

Fig. 14. Desired and synthesized linear group delay functions.

Fig. 11. Iteration 2 of the delay synthesis algorithm.
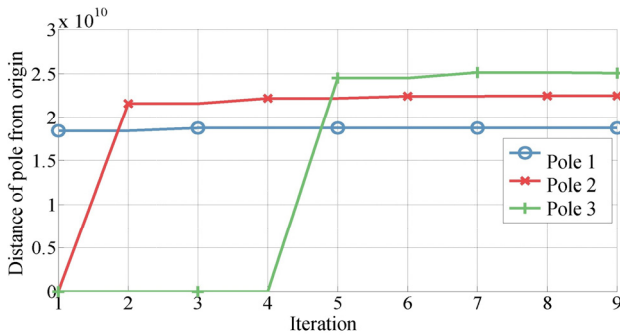
Fig. 15. Convergence of the pole components – measured as the distance of each respective pole from the origin of the s-plane.
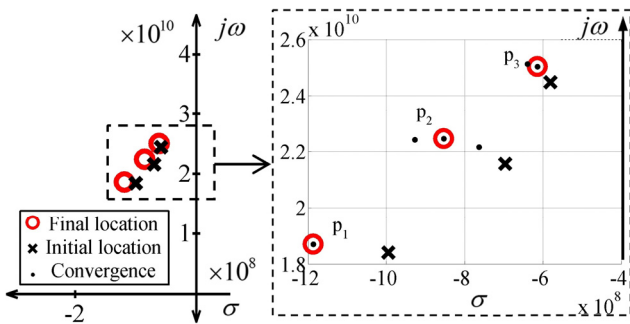

Fig. 16. Pole locations used to synthesize the linear delay function of Fig. 14. Pole locations: $p_1 = (-11.879, 1.870)$, $p_2 = (-8.535, 2.245)$, $p_3 = (-6.141, 2.503)$.

The resulting error function variation is 278 ps over the entire bandwidth whereas the specified variation was 300 ps. Agreement can be further improved by specifying a threshold criterion more stringent than $q = 3\%$.

In order to synthesize the desired linear all-pass network, the obtained poles (as shown in Fig. 16) can be used to calculate the all-pass quadrature pair locations by using the transformation in (3).

3.2 Example 2: Synthesis of Gaussian and Quadratic Delay Functions

We now proceed to synthesize more complicated examples, namely Gaussian and quadratic delay functions, with peak delays of 2 ns and 1 ns respectively, as shown in Fig. 17(a) and Fig. 18(a). The cost functions τ_c are constructed (desired variation of the error function is set to 130 ps and 80 ps respectively), resulting in the equi-ripple error curves τ_e as shown in Fig. 17(b) and Fig. 18(b). Synthesized pole locations are shown in Fig. 17(c) and Fig. 18(c), while their convergence to the final solution is further illustrated in Fig. 17(d) and Fig. 18(d). Finally, the resulting Gaussian delay approximation is shown in Fig. 17(a) and the quadratic approximation in Fig. 18(a).

To illustrate the numerical process of synthesizing the Gaussian delay response, iterations that produce new poles, are shown in Fig. 19. This illustrates the systematic approach of the proposed algorithm, where the error delay curve is effectively "stitched-up" into its final form by the inclusion of each subsequent second-order all-pass section. The accuracy of the approximation of Theorem 1 is confirmed by the correspondence of the dotted group delay curves (representing an approximate group delay using theorem 1) to the solid curves.

3.3 Example 3: Equalization of Measured BPF Group Delay Response with Circuit Co-simulation

The proposed algorithm is now demonstrated by reducing the delay variation of physical S-parameter measurements; in this case on a fifth-order coupled hairpin resonator BPF with a fractional bandwidth of 6.8% and magnitude and group delay responses as shown in Fig. 21(a-b). The generated ideal equalization poles are implemented separately in a circuit solver, using lumped-element second-order all-pass sections [9], as shown in Fig. 20.

The initial delay variation is measured as 4026 ps and a desired maximum variation of 1100 ps is set for the error function τ_e. This requirement results in a three-section equalizing all-pass network with parameter values as summarized in Tab. 2. A finite Q-factor of 400 is assumed for the inductors and capacitors. Values for the circuit elements are calculated directly from the theoretical second-order all-pass sections [9], [12], [18]. All of the individually tuned all-pass sections are cascaded in series (without further optimization) to obtain the final all-pass network as shown in Fig. 1. The equalized curves are shown in Fig. 21(a-b).

The size and accuracy of component values required in Tab. 2 rule out implementation with discrete surface mount devices. This is true, in general, for microwave filters operating at C-band frequencies [20]. However, the required values are feasible on-chip using MIM capacitors and spiral inductors [21]. Furthermore, in the microelectronic realization, the Q-factors of the inductors may be achieved by either active enhancement of on-chip coil inductors [22] or implementation of active inductors with gm-C type impedance inversion of fixed MIM capacitors [23], [24]. In both cases careful control of process tolerances (on-chip MIM capacitors have absolute and relative tolerances of ±25% and ±0.1% respectively), to ensure the desired group delay response, is necessary [21]. One approach is by means of post-production tunable CMOS varactors.

A resulting ripple of 1058 ps is obtained in Fig. 21(b). This is equivalent to a group delay variation reduction of 74% and 72% respectively.

The reduced group delay is achieved at the cost of a 2.3 dB insertion loss increase. This increase is, however, constant across the band, which is characteristic of dissipative resistive losses attributed to the finite Q-factor of the lumped elements. The effect of a finite Q-factor on the insertion loss and resulting group delay variation of the cascaded system is further illustrated in Fig. 23.
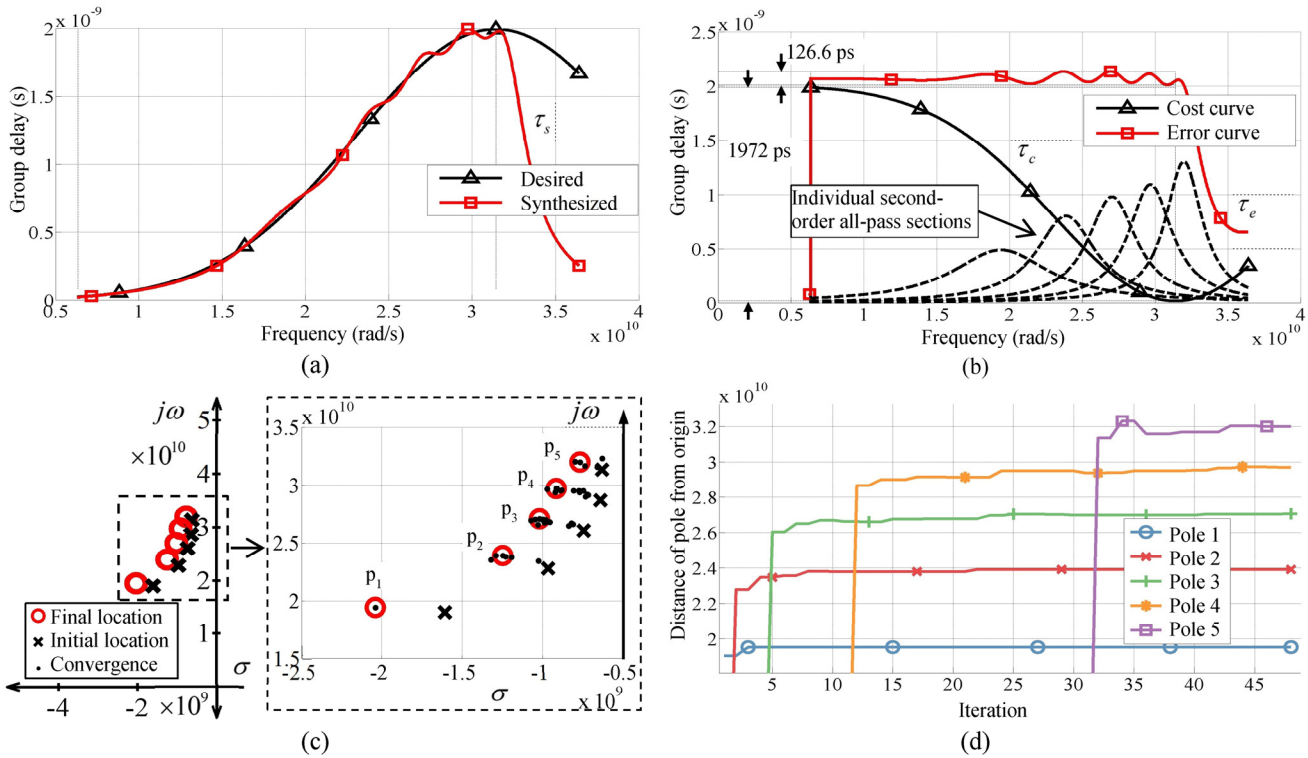
Fig. 17. (a) Desired Gaussian delay function and the synthesized 10th-order all-pass approximation thereof. (b) Group delay cost and error functions. (c) Pole locations: $p_1 = (-2.040, 1.942)$, $p_2 = (-1.247, 2.389)$, $p_3 = (-1.020, 2.706)$, $p_4 = (-0.915, 2.969)$, $p_5 = (-0.767, 3.198)$. (d) Convergence of the pole components – measured as the distance of each respective pole from the origin of the s-plane.
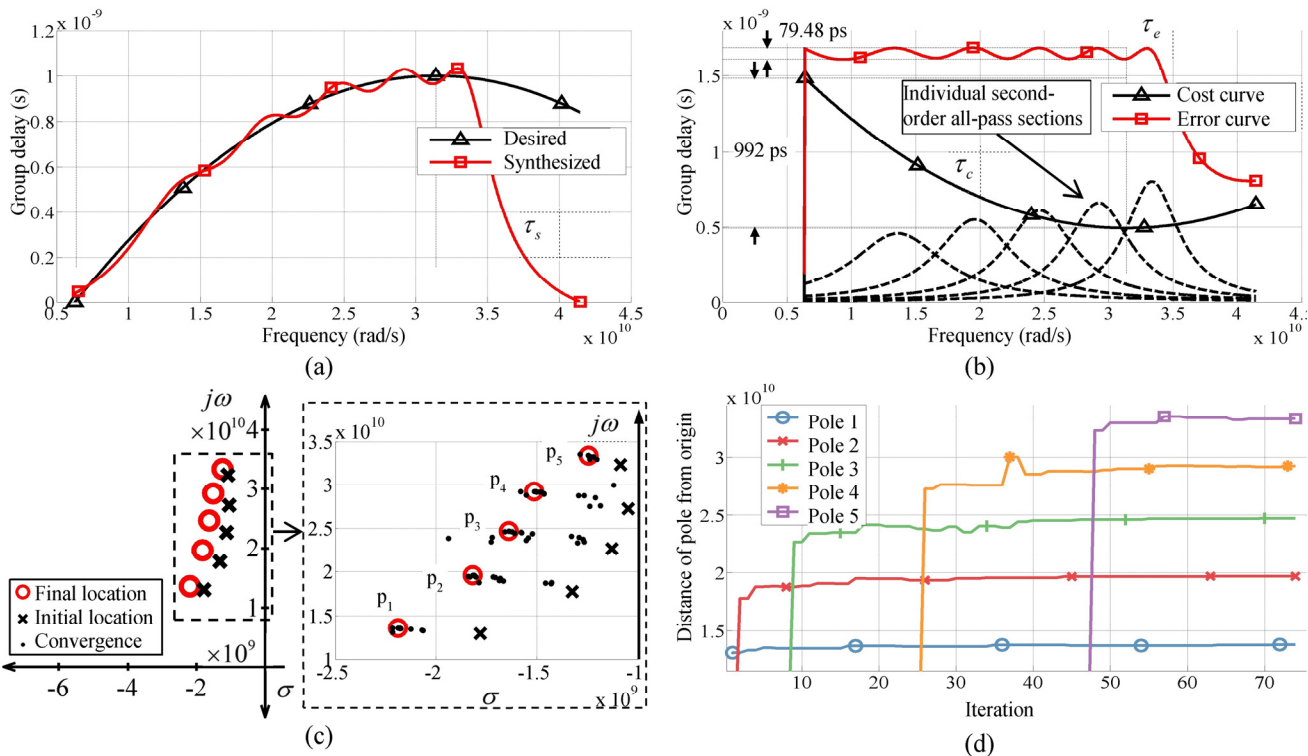

Fig. 18. (a) Desired quadratic delay function superimposed onto the synthesized 10th-order all-pass approximation. (b) Group delay cost and error functions. (c) Pole locations: $p_1 = (-2.188, 1.362)$, $p_2 = (-1.817, 1.960)$, $p_3 = (-1.639, 2.467)$, $p_4 = (-1.513, 2.923)$, $p_5 = (-1.244, 3.337)$. (d) Convergence of the pole components – measured as the distance of each respective pole from the origin of the s-plane.
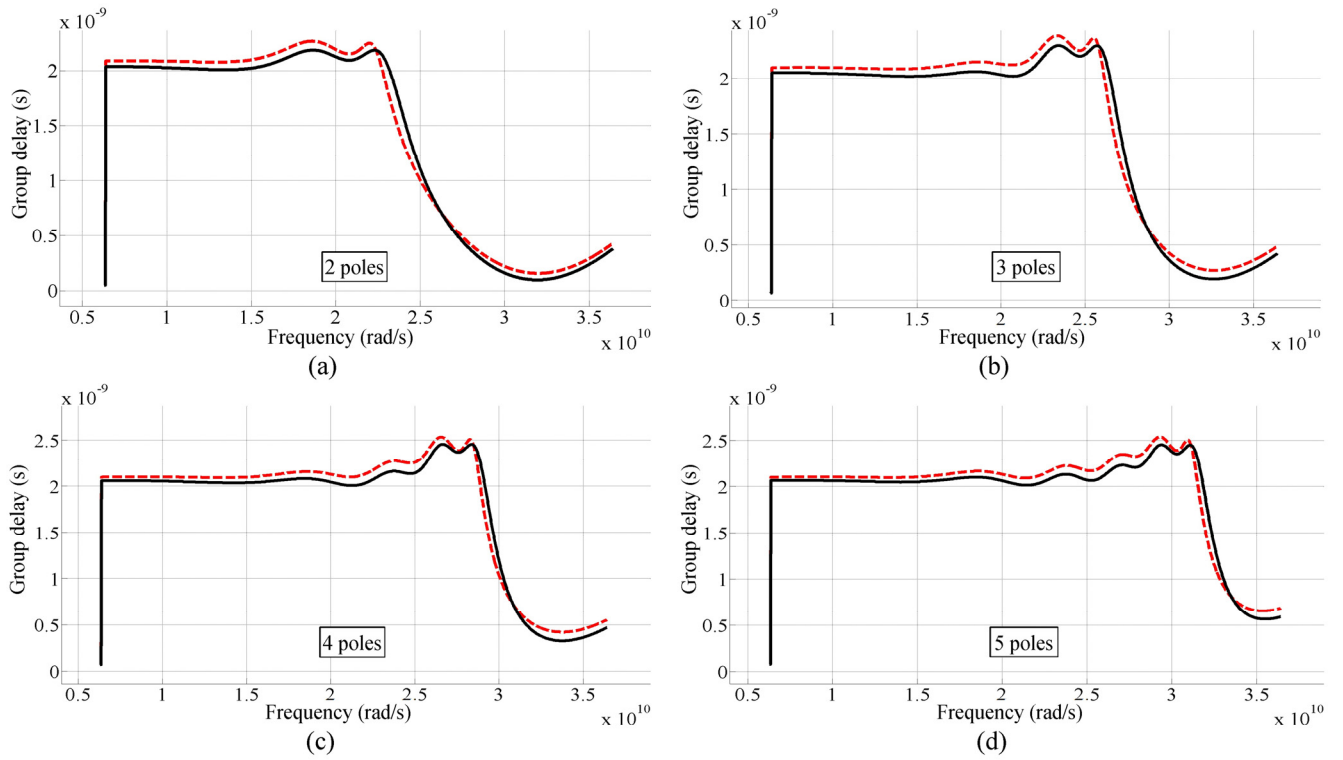
Fig. 19. Progression of the group delay synthesis algorithm at iterations: (a) 2; (b) 5; (c) 12; and (d) 32 as per Fig. 17 (d). Solid curves are obtained using (1), dotted curves using the approximation of theorem 1.
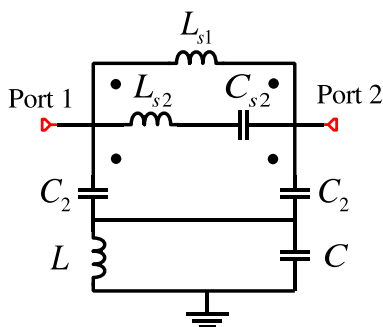

Fig. 20. Lumped-element second-order all-pass section.

Parameter	Section $\tau_{quad,x}$		
	1	2	3
L_{s1} / (pH)	354.4	352.4	433.3
L_{s2} / (pH)	766.1	757.2	936.1
C_{s2} / (pF)	1.273	1.226	0.9533
C_2 / (fF)	70.92	70.12	86.61
L / (nH)	3.178	3.071	2.376
C / (fF)	308.1	303.9	378.6

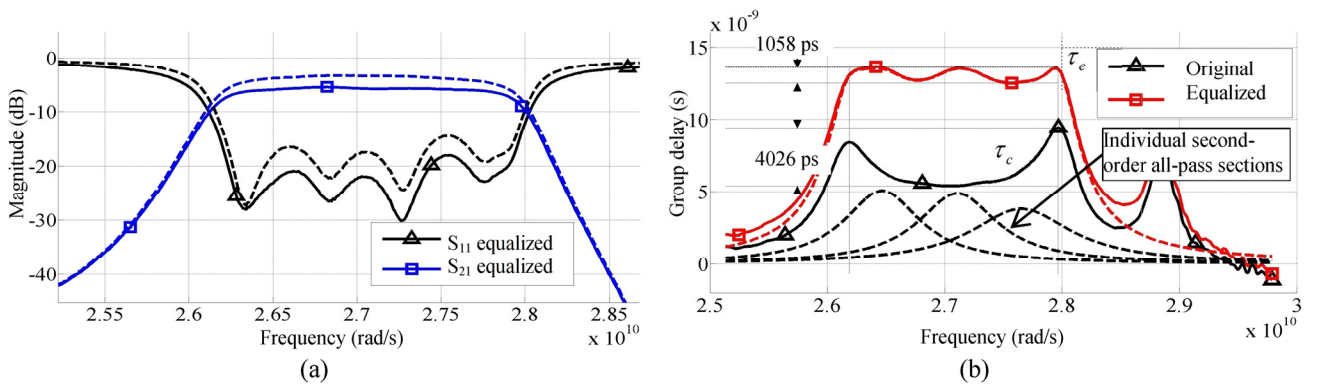**Tab. 2.** Parameter values for the three-element equalizing network.

Fig. 21. (a) Magnitude response of the initial (dotted curve) and equalized (solid curve) filter. (b) Original group delay measurement.
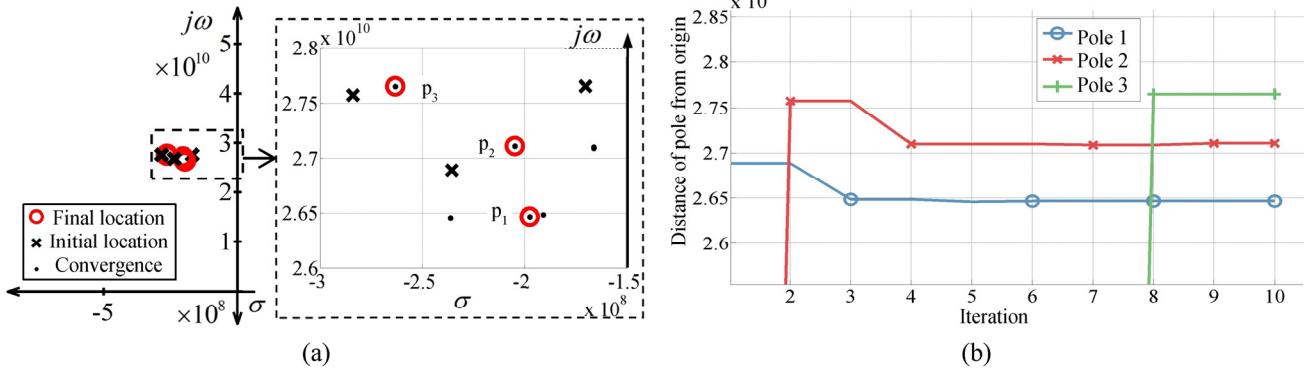
Fig. 22. Equalization pole locations: $p_1 = (-1.975, 2.647)$, $p_2 = (-2.049, 2.711)$, $p_3 = (-2.632, 2.765)$. (b) Convergence of the equalization pole components – measured as the distance of each respective pole from the origin of the s-plane.
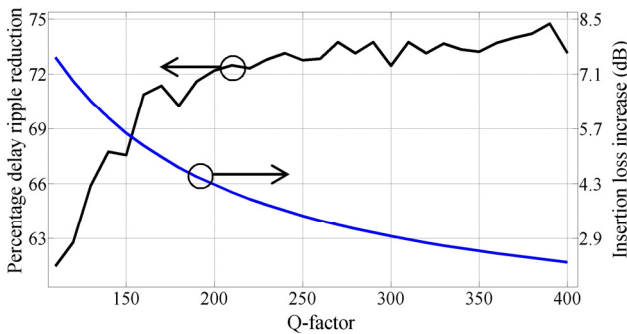

Fig. 23. Percentage delay variation reduction and insertion loss increase of the cascaded system as a function of the Q-factor.

The sixth-order equalizing all-pass network is synthesized in only 10 iterations due to the natural reduction in group delay variation experienced in practical filters because of finite resonator Q-factors.

4. Comparison of the Proposed Method with Existing Approaches

The Gaussian delay function synthesis (Fig. 17 (b)) and practical BPF delay equalization (Fig. 21 (b)) examples described above are repeated here, this time using existing approaches in literature, in order to illustrate the shortcomings stated in the introduction.

The methods in [1], [5], [6], [13], [16], require as input the desired number of poles as well as their starting locations. Here the starting values of the ω_x components are evenly sub-divided across the bandwidth of interest while the starting σ_x components are all set such as to create a peak delay equal to the maximum initial delay variation of the cost function. This choice can be justified by observing the pole locations synthesized in earlier examples.

Using this initial pole placement, the theoretical treatment presented in [13] is first applied to find an all-pass network for the Gaussian cost function (Fig. 17 (b)). No convergence could be obtained for any number of poles

without reducing the bandwidth by 16.6% (right-hand edge is removed). Fig. 24(a) shows the resulting group delay when five all-pass poles are used over this reduced bandwidth. A ripple of 786 ps is achieved over the originally specified passband as opposed to the 126.6 ps demonstrated in Sec. 3.2 using our proposed method.

In a similar manner an equalizing network is synthesized for the BPF delay response (Fig. 21 (b)), using two all-pass poles (no convergence could be obtained for three poles) as shown in Fig. 24(b).

The above two examples illustrate the following shortcomings associated with the approach in [13]:

1) There is no explicit control over the resulting maximum error delay variation.

2) Often the method does not converge to a solution (depending on the delay cost function and specified number of all-pass sections). In the preceding examples, this prevented the synthesis of the Gaussian delay to within the desired error ripple of 130 ps and the equalization of the BPF to within the specified ripple of 1100 ps, since the bandwidth and number of all-pass sections had to be adjusted to ensure convergence.

Numerical approaches aimed at finding optimal solutions in a large search space have gained prevalence in the modern group-delay synthesis literature [1], [5], [6], [14], [15], [16]. Here we will investigate two such approaches which are well suited to the synthesis problem, namely the genetic algorithm and simulated annealing technique. The maximum ripple of the error function is plotted versus the genetic algorithm generation in Fig. 24(c) and versus the simulated annealing iteration in Fig. 24(d), for a single run. A limit of 1000 generations and 2000 iterations are imposed on the two numerical algorithms. A solution is found to the BPF delay equalization problem after 100 generations (genetic algorithm) and 150 iterations (simulated annealing). On the other hand, an optimal Gaussian group delay response is not successfully synthesized – no improvement occurs after the 300th generation and the 400th iteration respectively.
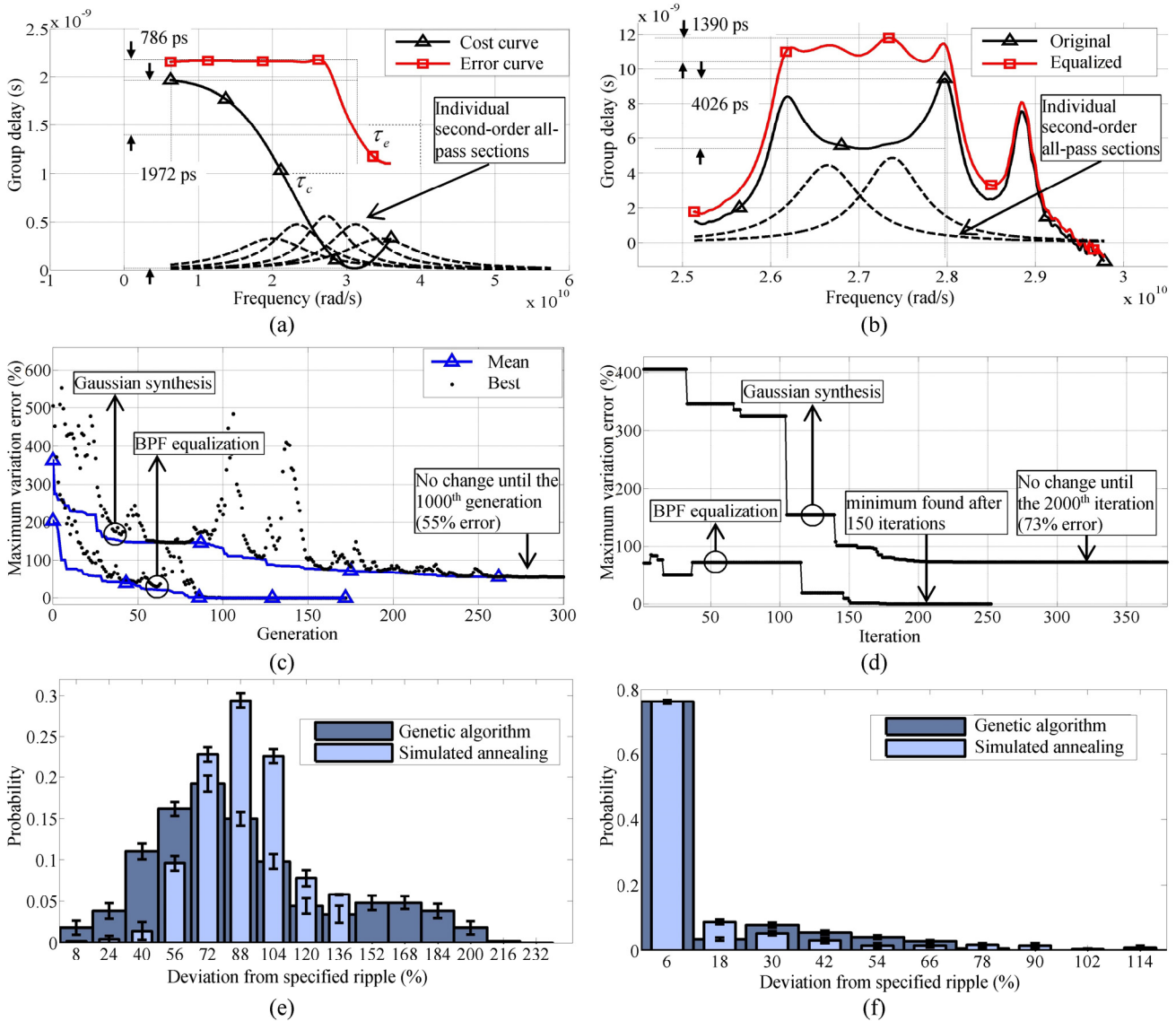
Fig. 24. (a) Cost and error group delay functions (Gaussian). (b) Initial and equalized group delay responses (practical BPF). (c) Genetic algorithm applied to the minimization of the Gaussian and BPF delay error functions. (d) Simulated annealing applied to the minimization of the Gaussian and BPF delay error functions. (e) Probability distribution of the deviation from the specified passband ripple for the Gaussian synthesis problem. (f) Probability distribution of the deviation from the specified passband ripple for the BPF delay synthesis problem.

It is important to note that separate runs converge to different end results, due to the random initial seed values intrinsic to the aforementioned algorithms. Probability distributions of maximum error ripples, for the aforementioned synthesis problems, as shown in Fig. 24(e) and Fig. 24(f), are computed from a sample of 500 separate runs. The standard deviation is shown for each bin. A limit of 1000 generations and 2000 iterations is imposed on the two numerical algorithms.

These results illustrate that convergence to a global optimum is a matter of finite probability and cannot be guaranteed (Figure 24(e) and 24(f) show the large number of local minima that typically exist in the search space). For example, in the Gaussian synthesis problem, 10 parameters are optimized. If each parameter is assigned to a subset of 100 points about the initial starting value then 10^{20} function evaluations are required to cover the entire search space. A simulation of 1000 generations requires roughly 20000 function evaluations, which covers only 2×10^{-16} of the search space. Further, the search space partitioning could be too course and fail to find the solution altogether.

Only 1.8% of the genetic algorithm solutions for the Gaussian synthesis problem are optimal. On the other hand, an optimum solution is found to the simpler BPF equalization problem 76% of the time. This might still be insufficient for certain applications, such as the adaptive delay equalization of a practical system.

The proposed method of this paper overcomes the aforementioned limitations by, in each case, converging to an optimal solution with an order of magnitude fewer iterations.

5. Conclusion

An analytically-based numerical method for synthesizing quasi-arbitrary group delay functions using minimum-order series-cascaded all-pass networks is presented. The method is compatible with any physical implementation of a second-order all-pass delay network and is shown to converge to a globally optimum, equi-ripple solution, requiring an order of magnitude fewer iterations than state-of-the-art methods. It is also shown that current methods relying on the genetic and simulated annealing algorithms do not always converge to a global optimum (as the proposed method does). As proof of concept, linear, quadratic and Gaussian delay functions are synthesized, to within any arbitrarily specified maximum error of approximation. The proposed method is further demonstrated by reducing the group delay variation of a physically measured fifth-order hairpin resonator BPF with 6.8% relative bandwidth, by 72%.

Acknowledgments

6. Appendix I

6.1 Derivation of Theorem 1

Consider a single pole in the s-plane as shown in Fig. 25. Point P_1 represents the location of the pole of interest. Points P_2 and P_4 are arbitrary locations on the Im $j\omega$-axis separated by a differential distance $\Delta\omega$. The group delay of a linear system described by an S-parameter matrix can be calculated from the S_{21} parameter as follows:

$$\tau \triangleq -\frac{\partial \measuredangle S_{21}}{\partial \omega}. \quad (15)$$

Equation (15) can be expressed as:

$$\tau = -\lim_{\Delta\omega \to 0} \frac{\Delta \measuredangle S_{21}}{\Delta\omega} = -\lim_{\Delta\omega \to 0} \frac{\Delta \theta_{21}}{\Delta\omega} \approx -\frac{-(\theta_2 - \theta_1)}{\Delta\omega}, \quad (16)$$

allowing the relationship between τ and the geometrical representation of Fig. 25.

As ω is traversed from P_2 to P_4 by the differential $\Delta\omega$, the angle $\measuredangle S_{21}$ increases by a corresponding differential amount. The ratio of these two differential changes is the group delay of S_{21}. The distance of P_1 from P_2 determines the resulting differential ratio, or group delay. With the aid of Fig. 26 and using the approximation presented in (16), we first find the relationship between $\Delta\theta$ and $\overline{P_2 P_3}$ as follows:
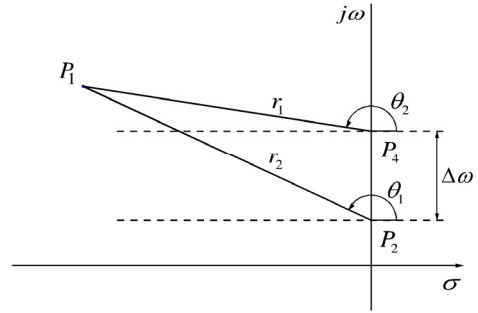

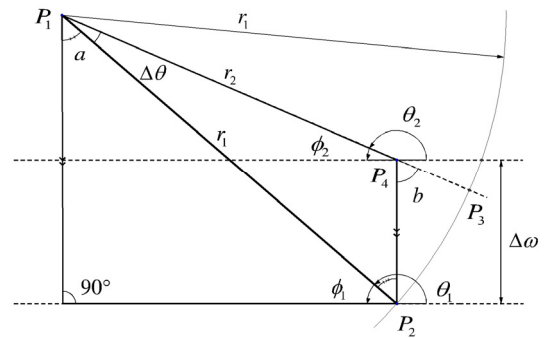**Fig. 25.** Geometry of the group delay response of a single pole.

Fig. 26. A geometrical representation of the group delay caused by a single pole.

$$\Delta\omega \to 0 \Rightarrow r_1 \to r_2 \Rightarrow r_1 \approx r_2 \approx r: \quad \widehat{P_2 P_3} = 2\pi r \frac{\Delta\theta}{2\pi},$$

$$\therefore \widehat{P_2 P_3} = r\Delta\theta: \quad \text{Since } \lim_{\Delta\omega \to 0} \widehat{P_2 P_3} = \overline{P_2 P_3} \Rightarrow \overline{P_2 P_3} \approx r\Delta\theta. \quad (17)$$

Next, a relationship between $\overline{P_2 P_3}$ and $\Delta\omega$ can be found:

$$\frac{\sin(\measuredangle b)}{\overline{P_2 P_3}} = \frac{\sin\left(\frac{\pi - \Delta\theta}{2}\right)}{\Delta\omega} \quad \text{(Sin rule)}$$

$$\therefore \Delta\omega = \frac{\overline{P_2 P_3} \sin\left(\frac{\pi - \Delta\theta}{2}\right)}{\sin(\measuredangle a + \Delta\theta)}. \quad (18)$$

In order to impose the required simplicity of this approximation it is assumed that $\measuredangle a \approx \pi/2$ rad. This implies that the approximation is only valid for $\omega \approx \omega_{px}$ (where ω_{px} is the imaginary component of the pole p_x at point P_1 in Fig. 26). The validity of the approximation is only important near this point − as justified by the requirement of (9) and (10). Therefore we may now write:

$$\overline{P_2 P_3} \approx \Delta\omega \Rightarrow \Delta\omega \approx \Delta\theta.r$$

$$\therefore \frac{\Delta\theta}{\Delta\omega} = \frac{1}{r}.$$

From (16):

$$\tau_{px} \approx \frac{1}{r} \blacksquare \quad (19)$$

6.2 Derivation of Theorem 2

Let $\omega = \omega_{mx}$ be the location of the xth desired local minimum of τ_e on the $j\omega$-axis. The frequency $\omega = \omega_{mx}$ is a local minimum or maximum if, and only if,

$$\frac{\partial}{\partial \omega}\big[\tau_e(\omega)\big]\bigg|_{\omega=\omega_{mx}} = -\frac{\partial}{\partial \omega}\big[\tau_{\text{quad},x}(\omega)\big]\bigg|_{\omega=\omega_{mx}}. \qquad (20)$$

Using theorem 1 we can replace the right hand side of (20) with $\tau_{\text{quad},x}(\omega) = 1/r_{px}$, where $r_{px} = \overline{P_1 P_2}$. Let:

$$\frac{\partial}{\partial \omega}\big[\tau_e(\omega)\big]\bigg|_{\omega=\omega_{mx}} = -c_1 \qquad (21)$$

where c_1 is a constant. From Pythagoras we know that:

$$r_{px}^{\;2} = \sigma_{px}^{\;2} + \big(\omega_{px}^{\;2} - \omega\big)^2. \qquad (22)$$

It therefore follows from (20) - (22):

$$-\frac{\partial}{\partial \omega}\bigg[\frac{1}{r_{px}}\bigg] = -\bigg[-\frac{1}{2}\Big\{\sigma_{px}^{\;2} + \big(\omega_{px}^{\;2} - \omega\big)^2\Big\}^{-\frac{3}{2}}.2.\big(\omega - \omega_{px}\big)\bigg]$$

$$\therefore -\frac{\partial}{\partial \omega}\bigg[\frac{1}{r_{px}}\bigg]\bigg|_{\omega=\omega_{mx}} = -\big(\omega_{px} - \omega_{mx}\big).\Big\{\sigma_{px}^{\;2} + \big(\omega_{px}^{\;2} - \omega_{mx}\big)^2\Big\}^{-\frac{3}{2}}$$

$$\therefore c_1 = \big(\omega_{px} - \omega_{mx}\big).\Big\{\sigma_{px}^{\;2} + \big(\omega_{px}^{\;2} - \omega_{mx}\big)^2\Big\}^{-\frac{3}{2}}. \qquad (23)$$

This equation can be rewritten as:

$$r_{px} = \bigg\{\frac{\omega_{px} - \omega_{mx}}{c_1}\bigg\}^{\frac{1}{3}}. \qquad (24)$$

In order to simplify this result, polar co-ordinates are introduced, where $\measuredangle \beta_x$ is defined as shown in Fig. 27.

Equation (24) may now be written as:

$$r_{px}^{\;3}.c_1 = \cos\big(\beta_x\big).r_{px} \Rightarrow r_{px} = \bigg\{0, \sqrt{\frac{\cos\big(\beta_x\big)}{c_1}}\bigg\} \;\blacksquare \qquad (25)$$

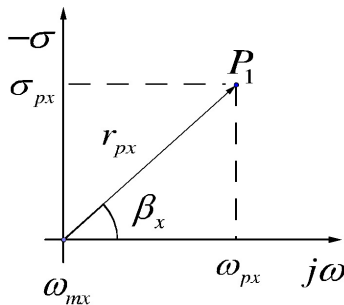where the first solution is trivial.

Fig. 27. Definition of $\measuredangle \beta_x$.

6.3 Derivation of (8)

A turning point is a local minimum if and only if $\tau''(\omega)$ is continuous at ω_{mx} and if both the following conditions are met (second derivative test): $\tau'(\omega)\big|_{\omega=\omega_{mx}} = 0$ and $\tau''(\omega)\big|_{\omega=\omega_{mx}} > 0$.

Since the first condition has already been satisfied (in theorem 2) the following restriction must be applied to ensure that the second condition is met:

$$\frac{\partial^2}{\partial \omega^2}\bigg[\Big\{\sigma_{px}^{\;2} + \big(\omega - \omega_{px}\big)^2\Big\}^{-\frac{1}{2}}\bigg] > c_2,$$
$$\text{where: } c_2 = -\frac{\partial^2}{\partial \omega^2}\big[\tau_e(\omega)\big]\bigg|_{\omega=\omega_{mx}}. \qquad (26)$$

The above may be re-written as:

$$\frac{2\omega_{mx}^{\;2} - 4\omega_{mx}\omega_{px} + 2\omega_{px}^{\;2} - \sigma_{px}^{\;2}}{\big[\omega_{mx}^{\;2} - 2\omega_{mx}\omega_{px} + \omega_{px}^{\;2} + \sigma_{px}^{\;2}\big]^{5/2}} > c_2. \qquad (27)$$

This expression can be simplified by using the polar coordinate representation:

$$\frac{\big[3\cos^2\big(\beta_{cx}\big) - 1\big].c_1^{\;3/2}}{\big[\cos\big(\beta_{cx}\big)\big]^{3/2}} > c_2 \;\blacksquare \qquad (28)$$

References

[1] GUPTA, S., PARSA, A., PERRET, E., et al. Group-delay engineered noncommensurate transmission line all-pass network for analog signal processing. *IEEE Transactions on Microwave Theory and Techniques,* 2010, vol. 58, no. 9, p. 2392–2407. ISSN: 0018-9480. DOI: 10.1109/TMTT.2010.2058933

[2] KERTIS, R., HUMBLE, J., DAUN-LINDBERG, M., et al. A 35 GS/s 5-Bit SiGe BiCMOS flash ADC with offset corrected exclusive-or comparator. In *IEEE 2008 Bipolar/BiCMOS Circuits and Technology Meeting.* Monterey (USA), 2008, p. 252–255. DOI: 10.1109/BIPOL.2008.4662755

[3] GUPTA, S., SOUNAS, D. L., ZHANG, Q., et al. All-pass dispersion synthesis using microwave C-sections. *International Journal of Circuit Theory and Applications,* 2014, vol. 42, no. 12, p. 1228–1245. DOI: 10.1002/cta.1916

[4] ZHANG, Q., GUPTA, S., CALOZ, C. Synthesis of broadband dispersive delay structures formed by commensurate C-and D-sections. *International Journal of RF and Microwave Computer-Aided Engineering,* 2014, vol. 24, no. 3, p. 322–331. DOI: 10.1002/mmce.20764

[5] ZHANG, Q., BANDLER, J. W., CALOZ, C. Design of dispersive delay structures (DDSs) formed by coupled C-sections using predistortion with space mapping. *IEEE Transactions on Microwave Theory and Techniques,* 2013, vol. 61, no. 12, p. 4040–4051. DOI: 10.1109/TMTT.2013.2287678

[6] ZISKA, P., LAIPERT, M. Band-pass filter group delay equalization. In *Proceeding of the Thirty-Eighth Southeastern*

Symposium on System Theory. Cookeville (USA), 2006, p. 483–487. DOI: 10.1109/SSST.2006.1619130

[7] OSUCH, P. J., STANDER, T. An on-chip post-production tunable group delay equaliser. In *International Conference on Actual Problems of Electron Devices Engineering (APEDE).* Saratov (Russia), 2014, p. 177–184. DOI: 10.1109/APEDE.2014.6958742

[8] WILSON, C., WARDORP, B. Strip-line group delay equalisers. In *1st European Microwave Conference.* London (England), 1969, p. 319–322. DOI: 10.1109/EUMA.1969.331885

[9] LEVY, R. Realization of practical lumped element all-pass networks for delay equalization of RF and microwave filters. *IEEE Transactions on Microwave Theory and Techniques,* 2011, vol. 59, no. 12, p. 3307–3311. DOI: 10.1109/TMTT.2011.2172809

[10] AL-HASHIMI, B., DUDEK, F., MONIRI, M. Current-mode group-delay equalisation using pole-zero mirroring technique. *IEE Proceedings - Circuits, Devices and Systems.* Stevenage (UK), 2000, p. 257–263. DOI: 10.1049/ip-cds:20000426

[11] FREDENALL, G. Delay equalization in color television. *Proceedings of the IRE,* 1954, vol. 42, no. 1, p. 258–262. ISSN: 0096-8390. DOI: 10.1109/JRPROC.1954.274635

[12] SCANLAN, S., RHODES, J. Microwave allpass networks–part I. *IEEE Transactions on Microwave Theory and Techniques,* 1968, vol. 16, no. 2, p. 62–72. DOI: 10.1109/TMTT.1968.1126610

[13] HELLERSTEIN, S. Synthesis of all-pass delay equalizers. *IRE Transactions on Circuit Theory,* 1961, vol. 8, no. 3, p. 215–222. ISSN: 0096-2007. DOI: 10.1109/TCT.1961.1086821

[14] CRANE, R. All-pass network synthesis. *IEEE Transactions on Circuit Theory,* 1968, vol. 15, no. 4, p. 474–478. DOI: 10.1109/TCT.1968.1082861

[15] VERGELLI, G., CHAKRABORTY, D. Computer-aided group delay equalization for broad-band satellite transponder applications. *IEEE Transactions on Communications,* 1973, vol. 21, no. 10, p. 1152–1156. DOI: 10.1109/TCOM.1973.1091553

[16] SAAL, R., ULBRICH, E. On the design of filters by synthesis. *IRE Transactions on Circuit Theory,* 1958, vol. 5, no. 4, p. 284–327. DOI: 10.1109/TCT.1958.1086481

[17] BUNKER, W. Symmetrical equal-ripple delay and symmetrical equal-ripple phase filters. *IEEE Transactions on Circuit Theory*, 1970, vol. 17, no. 3, p. 455–458. DOI: 10.1109/TCT.1970.1083107

[18] TSIVIDIS, Y. Integrated continuous-time filter design - an overview. *IEEE Journal of Solid-State Circuits,* 1994, vol. 29, no. 3, p. 166–176. DOI: 10.1109/4.278337

[19] POZAR, D. M. *Microwave Engineering.* Amherst (USA): John Wiley & Sons, 2009. ISBN: 978-0-470-63155-3.

[20] DALPATADU, R., MOUTHAAN, K. Active transversal S-band filter using lumped elements in standard 0.13 μm CMOS. In *The 7th German Microwave Conference.* Ilmenau (Germany), 2012, p. 1–4. ISBN: 978-1-4577-2096-3.

[21] FAYED, A., ISMAIL, M. *Adaptive Techniques for Mixed Signal System on Chip.* Dordrecht (The Netherlands): Springer, 2006. ISBN: 0-387-32154-3.

[22] YEONG-LIN LAI., CHUN-YI ZHENG. A novel folded active inductor for wireless communication SoC. In *2013 International SoC Design Conference.* Busan (South Korea), 2013, p. 306–309. DOI: 10.1109/ISOCC.2013.6864034

[23] SOORAPANTH, T., WONG, S. S. A 0-dB IL 2140±30 MHz bandpass filter utilizing Q-enhanced spiral inductors in standard CMOS. *IEEE Journal of Solid-State Circuits,* 2002, vol. 37, no. 5, p. 579–586. DOI: 10.1109/4.997850

[24] GEORGESCU, B., PEKAU, H., HASLETT, J., et al. Tunable coupled inductor Q-enhancement for parallel resonant LC tanks. *IEEE Transactions on Circuits and Systems II: Analog and Digital Signal Processing*, 2003, vol. 50, no. 10, p. 705–713. DOI: 10.1109/TCSII.2003.818366

About the Authors ...

Piotr Jan OSUCH was born in 1991, in Pretoria, South Africa. He received the Bachelors of Engineering (B.Eng) degree in Electronic Engineering from the University of Pretoria, South Africa, in 2013, and is currently working toward the Master of Engineering in Microelectronic Engineering (M.Eng) degree at the same university. There he is affiliated with the Carl and Emily Fuchs Institute for Microelectronics, where his current research interests lie in the synthesis of microwave filters with equalizing magnitude and group delay characteristics as well as the synthesis of quasi-arbitrary group delay elements and the microelectronic implementation of these networks. Mr. Osuch also serves as information security researcher at MWR InfoSecurity (PTY LTD) since 2014.

Tinus STANDER was born in Bellville, South Africa, in 1983. He completed his B.Eng and PhD degrees in Electronic Engineering at the University of Stellenbosch in 2005 and 2009, respectively. From 2010 to 2012 he served as RF and microwave engineer at Denel Dynamics (a division of Denel SOC LTD) before joining the Carl and Emily Fuchs Institute for Microelectronics (Dept. Electrical, Electronic and Computer Engineering) at the University of Pretoria in 2013. He currently serves as principal investigator in microwave and mm-wave microelectronics at the Institute, with a personal research interest in the application of distributed passives on-chip. He serves as a Chair of the SA IEEE AP/MTT/EMC chapter and faculty advisor to the University of Pretoria MTT-S student branch. He is also registered as Professional Engineer with the Engineering Council of South Africa.