

# Design and Optimization of a Novel Compact Broadband Linearly/Circularly Polarized Wide-Slot Antenna for WLAN and WiMAX Applications

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**Abstract.** *A novel topologically modified structure of a compact low profile wide-slot antenna for broadband applications is presented. The antenna comprises a modified E-shaped slot with unequal arm lengths in the ground plane, and a parasitic quasi-rectangular loop placed coplanar with the feedline. For exciting orthogonal modes with equal amplitude, a single-point feeding technique with an asymmetrical geometry of the coplanar waveguide is used to feed the antenna. A multi-stage EM-driven optimization is used to rigorously optimize all the parameters for best impedance bandwidth and axial ratio bandwidth. The total footprint of the antenna is only  $0.71 \lambda_g^2$  and a 41% impedance bandwidth along with 33% axial ratio bandwidth has been achieved which covers several WLAN and WiMAX bands.*

## Keywords

Broadband antenna, wide-slot antenna, circular polarization, WLAN antenna, WiMAX antenna, EM-driven optimization

## 1. Introduction

Recent trends in wireless communication systems create the needs for compact size components, stable communication links, as well as high-speed data transmission [1–4]. As planar broadband circularly polarized (CP) antennas with compact footprints and low profiles are capable of fulfilling these requirements, therefore development of high-performance CP structures has become a hot research topic. Compact size and planar geometry make them a viable choice for integration with microwave integrated circuits, whereas CP characteristics are especially suitable in the context of mitigating multipath losses, dropping signal interference, polarization mismatch, as well as reducing Faradays rotation effects [5–7]. For high-speed wireless data transmission, simultaneous multi-channel communication and improved sensitivity between the

transmitting and receiving antennas, a wide impedance bandwidth and axial ratio bandwidth (ARBW) of the antenna, are highly preferred.

Generally, CP polarization of the antenna can be attained with single point feeding but using this type of feeding with conventional geometry of the antenna can yield only a fraction of the impedance bandwidth. Similarly, if two-point feeding technique or addition active components are added to the circuit then it compromises the compactness of antenna and increases circuit complexity [8]. There are number of techniques that have been used for enhancing axial ratio bandwidth in particular [9], [10]. With the introduction of various topological modifications, an improvement in antenna performance (both in terms of electrical and field characteristics but also size reduction) can be obtained. However, these topological changes normally lead to increasing the structure complexity and hence a large number of geometrical parameters which have to be tuned. Unfortunately, most of the topologically modified planar antennas have a large number of parameters controlling the antenna performance figures such as impedance matching and axial ratio. Traditionally, the parameter sweeping techniques are used for optimizing all those adjustable parameters which is not an efficient approach both in terms of computational cost and also achieving a final finest design. To ensure optimum performance, rigorous numerical optimization of all antenna parameters is necessary, which, for the sake of reliability, has to be executed at the level of full-wave EM simulation models. This can be realized using conventional gradient-based algorithms [11], or, for improved computational efficiency, using surrogate-assisted techniques [12].

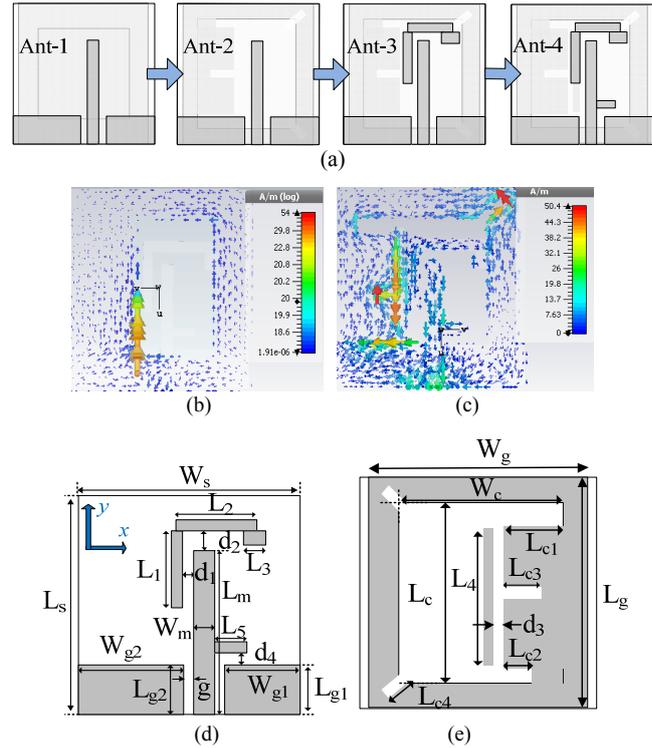
In this paper, a novel geometry of a planar, compact size and broadband linearly/circularly polarized wide slot antenna is presented. The key features of wide impedance bandwidth and ARBW are achieved using four-stage topology evolution of the proposed antenna. A square wide-slot antenna with a compact geometry of  $25 \times 25 \text{ mm}^2$  is used as a baseline design which is well-known for its wide impedance bandwidth and ARBW performance [13]. Sys-

tematic topological modification is introduced at the periphery of the wide-slot etched in the ground plane for exciting additional CP modes and broadening the ARBW. The major performance figures, i.e. impedance bandwidth and ARBW, are further improved through rigorous EM-driven optimization of relevant geometry parameters. For a computationally efficient optimization, the adjustable variables are subdivided based on a thorough sensitivity analysis. In the first stage of optimization, the most sensitive variables are optimized followed by repeating the same optimization routine for the whole set of variables. Numerical results are validated experimentally with a close agreement between simulation and measurement results. Finally, a comprehensive benchmarking is carried out indicating advantages of the proposed antenna over state-of-the-art designs reported in the literature.

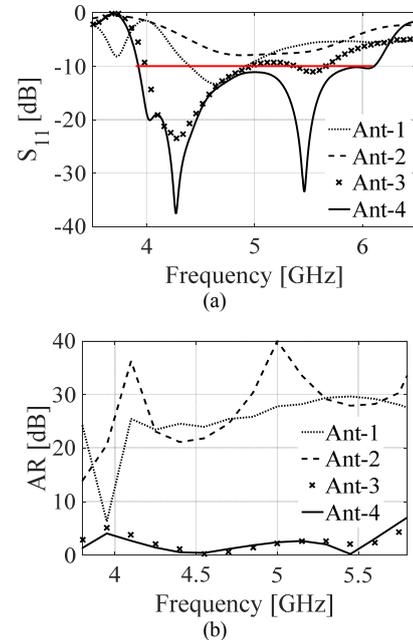
## 2. Antenna Configurations and Design Steps

The proposed antenna is designed on a laminated Rogers substrate RO4003C that has permittivity of 3.38, tangent loss 0.0027, and thickness of 0.813 mm. In step one, a wide square slot antenna was designed which is fed by an asymmetric coplanar waveguide (CPW) as shown in Fig. 1(a). The length  $L_m$  of the microstrip-line monopole, extending from the CPW, was kept to approximately  $\lambda/4$  at the center operating frequency (with respect to the impedance bandwidth) of the antenna. In the second step, the geometry of the square slot was modified, and a perturbation was introduced to enable generation of the orthogonal current distribution on the contour of the slot. The final design of the slot after the perturbation is of an E-shape with unequal arm lengths, which primarily contributes to the excitation of the orthogonal modes. In the conventional slot, the current only flows in one direction, along the  $y$ -plane, as shown in Fig. 1(b). By introducing a perturbation of unequal length extends, the current path and the  $y$ -plane as well as asymmetric current components in the  $x$ -plane are also generated at the slot contour as illustrated in Fig. 1(c). The magnitude of the asymmetric current in the  $xy$ -plane is almost of equal magnitude but shifted  $90^\circ$  in phase, which allows for generating additional CP modes. To achieve sufficient ARBW, a quasi-rectangular loop of a length equivalent to  $\lambda/4$  (at a lower cutoff frequency), is placed coplanar to the monopole. This parasitic component directs the current in the horizontal and vertical plane and, therefore, induces CP.

The final design step consists of adding another parasitic metallic strip within the wide slot in the ground plane, and a small impedance matching stub to the feed-line monopole. The main contribution of this step is improving the impedance matching by lengthening the current path which, as shown in Fig. 2, enhances both the impedance bandwidth and ARBW of the proposed antenna. The length of the parasitic strips and slots used in the proposed design are indicated with  $L_n$  and  $L_{cn}$  while their corresponding widths



**Fig. 1.** Antenna evaluation stages and final parametrized geometry: (a) Evolution stages of the proposed antenna. (b) Surface current distribution on conventional slot. (c) Surface current distribution on perturbed slot. (d) Parametrized front view. (e) Parametrized back view.



**Fig. 2.** Simulated characteristics of the optimized design of antenna of Fig. 1. (a) Reflection responses at four evolution stages. (b) Axial ratio characteristics at four evolution stages.

are represented as  $W_n$  and  $W_{cn}$ , where,  $n=1, 2, 3, \dots$ . The four evolution stages and the final parameterized design are depicted in Fig. 1. The geometrical size of the proposed

antenna is  $25 \text{ mm} \times 25 \text{ mm}$  (the footprint of only  $625 \text{ mm}^2$ ), see also Tab. 1.

## 2.1 Design Problem and Optimization Algorithm

Appropriate optimization of antenna geometry parameters is critical for achieving the best possible performance. Here, a multi-stage process is utilized which includes the following steps. For the purpose of description, the antenna impedance bandwidth will be denoted as  $BW_S(\mathbf{x})$  (i.e., the continuous frequency range for which  $|S_{11}| \leq -10 \text{ dB}$ ), whereas  $S(\mathbf{x})$  will denote the maximum reflection level within the proposed antenna frequency range. Also, we use the symbol  $AR(\mathbf{x})$  to denote the maximum value of axial ratio (AR) within the same frequency range. An explicit dependence on adjustable parameter vector  $\mathbf{x}$  is indicated to facilitate further description.

The design specifications are as follows:

- Ensure that  $S(\mathbf{x}) \leq -10 \text{ dB}$ ;
- Maximize  $BW_S(\mathbf{x})$  around 5 GHz;
- Minimize  $AR(\mathbf{x})$ .

Generally, straightforward optimization of all parameters with respect to all specifications fails due to several issues which include: (i) high cost of EM simulation of the antenna structure, (ii) a large number of geometrical parameters, and (iii) the necessity of simultaneous handling of several performance figures. To alleviate these problems, a multi-stage procedure is utilized as described below. The generic optimization task is formulated as follows:

$$\mathbf{x}^* = \arg \min_{\mathbf{x}} U(BW_S(\mathbf{x}), S(\mathbf{x}), AR(\mathbf{x})) \quad (1)$$

where  $U$  is the objective function. We consider two separate sub-problems. The antenna impedance bandwidth optimization is the first step for which the objective function is defined as:

$$U_S(BW_S(\mathbf{x}), S(\mathbf{x}), AR(\mathbf{x})) = -BW_S(\mathbf{x}) + \beta_S c_S(S(\mathbf{x}))^2 \quad (2)$$

in which  $c_S(S(\mathbf{x})) = \max\{(S(\mathbf{x}) + 10.0)/10\}$  is a penalty function that “measures” a relative violation of the condition  $S(\mathbf{x}) \leq -10 \text{ dB}$ , and  $\beta_S$  is a penalty factor.

The purpose of solving (1) with the objective function (2) is to increase the antenna bandwidth and to ensure sufficient impedance matching within the antenna operational bandwidth.

The objective function for the second sub-problem where the goal is to minimize the axial ratio bandwidth below 3 dB, is defined as:

$$U_{AR}(BW_S(\mathbf{x}), S(\mathbf{x}), AR(\mathbf{x})) = AR(\mathbf{x}) + \beta_S c_S(S'(\mathbf{x}))^2. \quad (3)$$

The symbol  $S'(\mathbf{x})$  denotes the maximum reflection level within the bandwidth obtained upon solving (1) with the objective function (2).

Furthermore, in order to facilitate the optimization process, sensitivity analysis was performed to identify the parameters with respect to which both design goals i.e.  $|S_{11}|$  and  $AR$  are the most sensitive. The twelve selected variables are denoted as  $\mathbf{x}_0 = [L_1 W_1 L_2 W_2 L_3 W_3 L_4 W_4 L_{g2} d_1 d_2 d_3]^T$ . The remaining variables are included in the second design stage.

The optimization process was carried out with the following steps:

1. Solve the problem (1) with the objective function (2) for a reduced parameter set  $\mathbf{x}_0$ :

$$\mathbf{x}_0^* = \arg \min_{\mathbf{x}} U_S(BW_S(\mathbf{x}_0), S(\mathbf{x}_0), AR(\mathbf{x}_0)).$$

2. Starting from  $\mathbf{x}_0^*$ , solve the problem (1) with the objective function (3) for a reduced parameter set:

$$\mathbf{x}_0^{**} = \arg \min_{\mathbf{x}} U_{AR}(BW_S(\mathbf{x}_0), S(\mathbf{x}_0), AR(\mathbf{x}_0)).$$

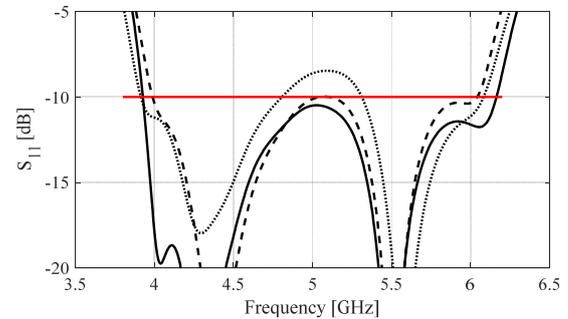
3. Solve the problem (1) with the objective function (2) for the entire parameter set (the components of  $\mathbf{x}_0^{**}$  are used as initial values):

$$\mathbf{x}^* = \arg \min_{\mathbf{x}} U_S(BW_S(\mathbf{x}), S(\mathbf{x}), AR(\mathbf{x})).$$

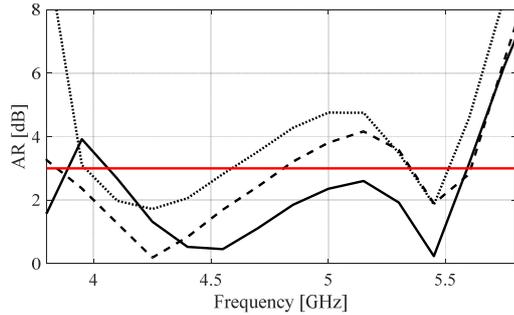
4. Identify the final design by solving (1) with the objective function (3) for the entire parameter set, starting from  $\mathbf{x}^*$ :

$$\mathbf{x}^{**} = \arg \min_{\mathbf{x}} U_{AR}(BW_S(\mathbf{x}), S(\mathbf{x}), AR(\mathbf{x})).$$

All sub-problems are solved using a trust-region gradient search [14] with the antenna response gradients estimated using finite differentiation. Sequential optimization (first for impedance bandwidth enhancement, then for axial ratio improvement) allows for efficient handling of all performance figures. In particular, ensuring sufficient matching provides a feasible starting point for AR optimization. The results of three stage optimization are depicted in term of impedance matching and AR in Fig. 3 and Fig. 4 respectively. The initial design values are obtained based on classic antenna theory. As can be seen from reflection



**Fig. 3.** Reflection response of the antenna of Fig. 1 at various stages of the design process: initial design (····), optimization with reduced parameter set  $\mathbf{x}_0^{**}$  (- - -), final design  $\mathbf{x}^{**}$  (—). Bandwidth of interest and  $-10 \text{ dB}$  level marked with vertical and horizontal lines, respectively.



**Fig. 4.** Axial ratio of the antenna of Fig. 1 at various stages of the design process: initial design (····), optimization with reduced parameter set  $\mathbf{x}_0^{**}$  (- - -), final design  $\mathbf{x}^{**}$  (—). Bandwidth of interest and 3 dB level marked with vertical and horizontal lines, respectively.

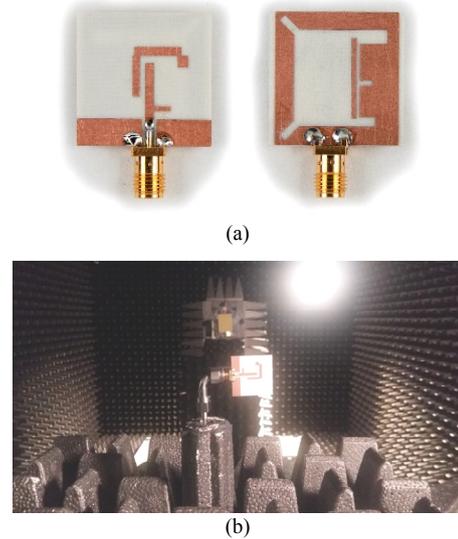
<b>Parameter</b>	$L_s$	$W_s$	$L_g$	$W_g$	$L_{g1}$	$W_{g1}$
<b>Value (mm)</b>	25	25	25	23	5	10.12
<b>Parameter</b>	$L_{g2}$	$W_{g2}$	$L_m$	$W_m$	$L_1$	$W_1$
<b>Value (mm)</b>	5.11	12.12	15.5	1.55	7.55	1.3
<b>Parameter</b>	$L_2$	$W_2$	$L_3$	$W_3$	$L_4$	$W_4$
<b>Value (mm)</b>	8.7	1.7	2.18	1.95	3.12	0.94
<b>Parameter</b>	$L_c$	$W_c$	$L_{c1}$	$W_{c1}$	$L_{c2}$	$W_{c2}$
<b>Value (mm)</b>	17.96	16.4	5.13	2.63	2.87	1.69
<b>Parameter</b>	$L_{c3}$	$W_{c3}$	$L_{c4}$	$W_{c4}$	$g$	$d_1$
<b>Value (mm)</b>	2.37	0.91	3.12	1.37	0.6075	1.656
<b>Parameter</b>	$d_2$	$d_3$	$d_4$	$L_5$	$W_5$	
<b>Value (mm)</b>	1.03	0.57	1.56	3.12	0.94	

**Tab. 1.** Parameter values of the proposed CP antenna.

coefficient response of the antenna, for the initial design the impedance matching is way above  $-10$  dB reference line. After the first stage optimization of most sensitive variables, both impedance matching and axial ratio are improved and reach near the reference line at  $-10$  dB and 3 dB respectively. After performing the final optimization for the whole set of variables the responses are further improved and the primary goal of well-matched antenna is achieved. It is important to mention here that a compact physical size of the antenna is maintained to  $25 \times 25$  mm<sup>2</sup>. It is very challenging to achieve a wide impedance bandwidth and axial ratio bandwidth with the traditionally used optimization techniques.

### 3. Experimental Verification and Benchmarking

The final design of the proposed antenna has been fabricated and measured. Figure 5 shows the photograph of the antenna prototype and the experimental setup for characterizing the proposed antenna. Similarly, a comparison of simulated and measured reflection response, axial ratio, and realized gain (both in a broadside direction) is illustrated



**Fig. 5.** Experimental validation of the proposed CP antenna: (a) Photographs of the antenna prototype (front – left, back – right). (b) Experimental setup.

in Fig. 6. An impedance bandwidth of 44% (3.9 GHz to 6.2 GHz) is achieved with a 34% ARBW while a compact geometry of the antenna is maintained. Furthermore, the antenna exhibits a stable gain response throughout the operating band and the average realized gain of the antenna is 3.62 dB. The impedance bandwidth and axial ratio bandwidth response shows that the antenna can be used for several applications around 5 GHz frequency which include WLAN and WiMAX band.

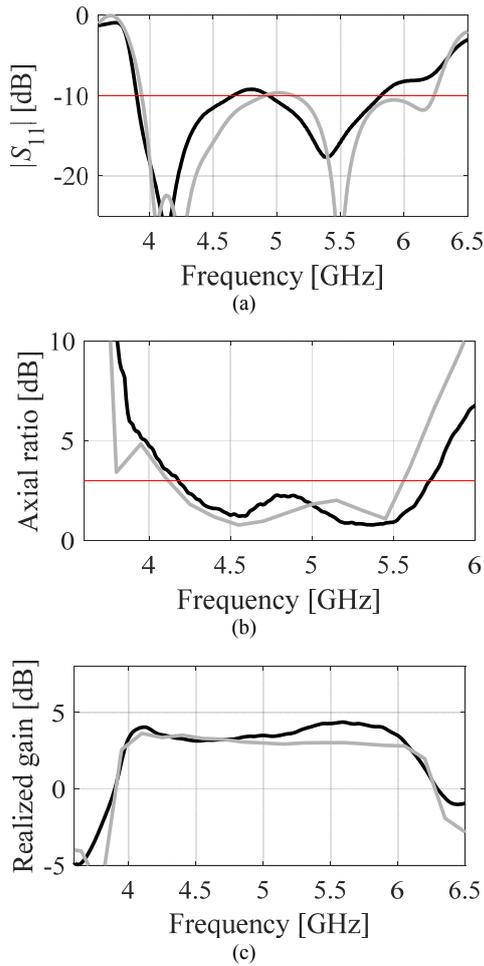
Figure 7 shows the LHCP and RHCP radiation patterns of the antenna in  $xz$ -plane. Similarly, Figure 8 depicts the simulated and measured  $xy$ -plane. A bidirectional radiation pattern with good agreement between simulation and measurement is observed. Slight discrepancies originate from fabrication/assembly inaccuracies and mechanical instabilities.

## 4. Benchmarking

The proposed antenna has been compared in terms of ARBW, impedance bandwidth, and footprint to several state-of-the-art CP antennas recently reported in the literature. The structures operating within similar frequency ranges have been selected. For the sake of fair comparison, the antenna sizes were expressed in terms of the guided wavelength ( $\lambda_g$ ). Table 2 indicates that the proposed antenna exhibits better performance with respect to all major performance figures, including impedance bandwidth, ARBW, and the size.

## 5. Conclusion

The article proposes a novel structure of a compact low profile wide-slot CP antenna. A multi-stage optimization routine is developed and implemented for rigorously

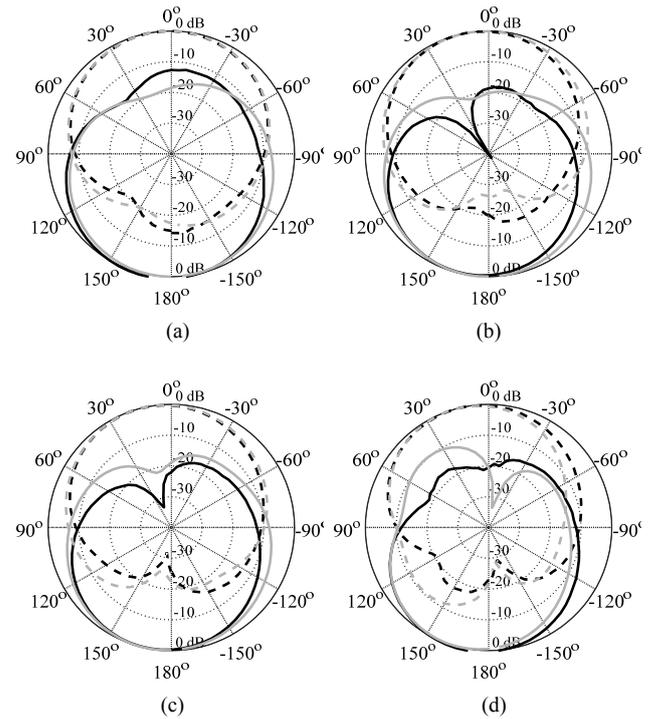


**Fig. 6.** Experimental validation of the proposed CP antenna: (a) Simulated (gray) and measured (black) reflection responses. (b) Simulated (gray) and measured (black) axial ratio characteristics. (c) Simulated (gray) and measured (black) realized gain characteristics.

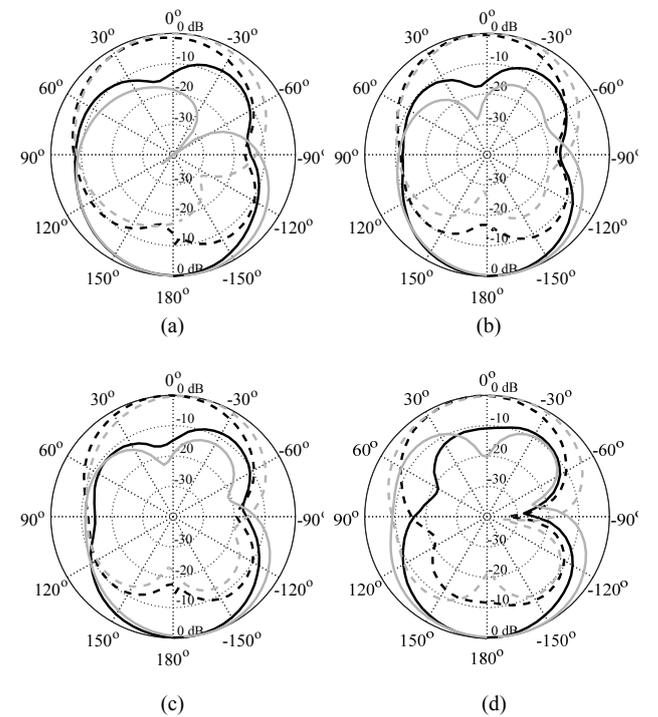
Ref.	% AR <sup>s</sup>	% IBW <sup>*</sup>	Antenna footprint		Year
			mm <sup>2</sup>	$\lambda_g^2$ #	
[15]	27	111	2500	1.58	2013
[16]	15.4	----	900	0.95	2010
[17]	26.9	27	2500	1.58	2017
[18]	14	27	400	0.63	2015
[19]	30	51	19158	1.44	2013
[20]	22	37	2500	2.00	2015
[21]	22.2	28.6	2025	54.56	2017
This work	33	41	625	0.71	2018

**Tab. 2.** Comparison with state-of-the-art CP antennas. <sup>s</sup> % AR stands for fractional axial ratio bandwidth, <sup>\*</sup> % IBW stands for fractional impedance bandwidth, #  $\lambda_g^2$  denotes the antenna footprint in terms of the guided wavelength.

optimizing all adjustable parameters. The final optimized design is then prototyped and characterized in anechoic chamber. The antenna features 33-percent axial ratio bandwidth and 41-percent impedance bandwidth as well as a small size of only 25 mm × 25 mm. The operational range covers several WLAN and WiMAX bands. Comprehensive benchmarking indicates that the proposed antenna



**Fig. 7.** Simulated (grey) and measured (black) radiation patterns obtained for the proposed antenna in the  $xz$  plane. RHCP and LHCP patterns are shown using solid and dashed lines, respectively (a) 4.2 GHz, (b) 4.9 GHz, (c) 5.2 GHz, (d) 5.5 GHz.



**Fig. 8.** Simulated (grey) and measured (black) radiation patterns obtained for the proposed antenna in the  $xy$  plane. RHCP and LHCP patterns are shown using solid and dashed lines, respectively (a) 4.2 GHz, (b) 4.9 GHz, (c) 5.2 GHz, (d) 5.5 GHz.

exhibits competitive performance compared to state-of-the-art structures from the literature.

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